

**ENCE 355 – Introduction to Structural Design**  
**SOLUTIONS to Homework Set No. 11**  
**Fall 2002**

PROB # 3-34

Using a W12x45 ( $A_g = 13.1 \text{ in.}^2$ ,  $d = 12.1 \text{ in.}$ ,  
 $b_f = 8.05 \text{ in.}$ ,  $t_f = 0.575 \text{ in.}$ )

$F_y = 50 \text{ ksi}$  and  $F_u = 70 \text{ ksi}$  from Manual Table 2-1

$$\phi_t P_n = \phi_t F_y A_g = (0.9)(13.1)(50) = 589.5 \text{ k}$$

$$A_m = 13.1 - (4)\left(\frac{7}{8}\right)(0.575) = 11.09 \text{ in.}^2$$

$$\bar{x} = \bar{y} \text{ for a WT6x22.5} = 1.13 \text{ in.}$$

$$u = 1 - \frac{\bar{x}}{L} = 1 - \frac{1.13}{6} = 0.812 < 0.9 \text{ ok}$$

$$\phi_t P_n = (0.75)(70)(0.812 \times 11.09) = 472.8 \text{ k} \leftarrow$$

Checking block shear

$$A_{gv} = (4)(8)(0.575) = 18.40 \text{ in.}^2$$

$$A_{gt} = (4)(1.275)(0.575) = 2.93 \text{ in.}^2$$

$$A_{mv} = (4)\left(8 - 2.5 \times \frac{7}{8}\right)(0.575) = 13.36 \text{ in.}^2$$

$$A_{mt} = (4)\left(1.275 - \frac{1}{2} \times \frac{7}{8}\right)(0.575) = 1.93 \text{ in.}^2$$

$$0.6 F_u A_{mv} = (0.6)(70)(13.36) = 561.2 \text{ k}$$

$$> F_u A_{mt} = (70)(1.93) = 135.1 \text{ k}$$

$\therefore$  Use LRFD Equation J4-36

$$\phi R_n = \phi [0.6 F_u A_{mv} + F_y A_{gt}] = 0.75 [561.2 + (50)(2.93)]$$

$$= 530.8 \text{ k} \leq 0.75 [(0.6)(70)(13.36) + (70)(1.93)] = 522.1 \text{ k}$$

$\text{Ans.} = 472.8 \text{ k}$

$\checkmark$  JCM

PROB # 4-3

$$(1) \min A_g = \frac{P_u}{\phi_t F_y} = \frac{380}{(0.9)(50)} = 8.44 \text{ in.}^2$$

$$(2) \min A_g = \frac{P_u}{\phi_t F_u u} + \text{estimated area of holes}$$

Assume  $u = 0.9$  and flange  $t = 0.515 \text{ in.}$

$$\min A_g = \frac{380}{(0.75)(65)(0.9)} + (4)\left(\frac{7}{8}\right)(0.515) = 10.46 \text{ in.}^2 \leftarrow$$

$$(3) \text{ Preferable } \min \lambda = \frac{L}{300} = \frac{(12)(28)}{300} = 1.12 \text{ in.}^2$$

Try W12x40 ( $A_g = 11.7 \text{ in.}^2$ ,  $t_f = 0.515 \text{ in.}$ ,  $\lambda_y = 1.94 \text{ in.}$ )

$$\phi_t P_m = (0.9)(50)(11.7) = 526.5 \text{ k} > 380 \text{ k} \quad \underline{\text{OK}}$$

$$\bar{x} = \bar{y} = 1.09 \text{ in for a WT6x20}$$

$$u = 1 - \frac{\bar{x}}{L} = 1 - \frac{1.09}{8} = 0.864 < 0.9 \quad \underline{\text{OK}}$$

$$A_m = 11.7 - (4)\left(\frac{7}{8}\right)(0.515) = 9.90 \text{ in.}^2$$

$$\phi_t P_m = (0.75)(65)(0.864)(9.90) = 417 \text{ k} > 380 \text{ k} \quad \underline{\text{OK}}$$

$$\frac{L}{\lambda} = \frac{(12)(28)}{1.94} = 173 < 300 \quad \underline{\text{OK}}$$

**USE W12x40**

✓  $\phi_t P_m \leq$

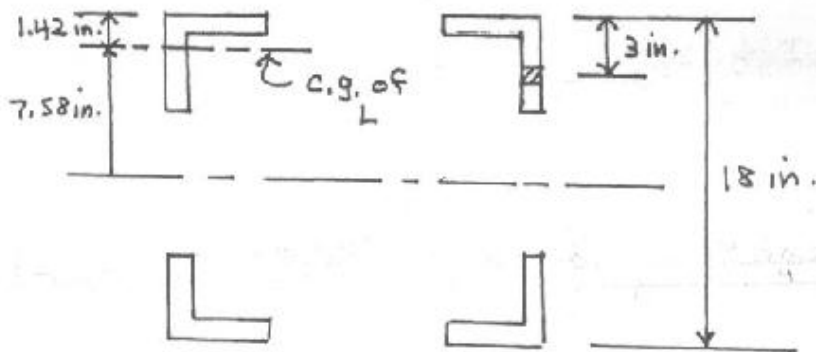
PROB # 4-23 (1)

$$P_u = (1.2)(180) + (1.6)(320) = 728 \text{ k}$$

$$\text{Min } A_g = \frac{P_u}{\phi_t F_y} = \frac{728}{(0.9)(50)} = 16.18 \text{ in.}^2$$

$$\text{Min } A_m = \frac{P_u}{\phi_t F_u} = \frac{728}{(0.75)(65)(1.0)} = 14.93 \text{ in.}^2$$

Angle t (in)	Area of 8 1-in. holes (in. <sup>2</sup> )	A <sub>g</sub> reqd (in. <sup>2</sup> )	Angles
7/16	3.50	18.43	4Ls 6x6x 7/16 (5.08 in. <sup>2</sup> )
1/2	4.00	18.93	4Ls 5x5x 1/2 (4.79 in. <sup>2</sup> each)
9/16	4.50	19.43	4Ls 6x4x 9/16 (5.27 in. <sup>2</sup> each)
5/8	5.00	19.93	4Ls 5x5x 5/8 (5.90 in. <sup>2</sup> each)



PROB # 4-23 (2)

$$A = (4)(4.79) = 19.16 \text{ in.}^2$$

$$I_x = I_y = 4 [11.3 + (4.79)(7.58)^2] = 1146 \text{ in.}^4$$

$$r = \sqrt{\frac{1146}{19.16}} = 7.73 \text{ in.}$$

$$\frac{L}{r} = \frac{(12)(30)}{7.73} = 46.6 < 300 \text{ OK}$$

Design of tie plates

$$\text{Distance between bolt lines} = 18 - (2)(3) = 12 \text{ in.}$$

$$\text{Min length} = \left(\frac{2}{3}\right)(12) = \underline{8 \text{ in.}}$$

$$\text{Min width} = 12 + (2)\left(1\frac{1}{2}\right) = \underline{15 \text{ in.}}$$

$$\text{Min } t = \left(\frac{1}{50}\right)(12) = 0.24 \text{ in. Say } \underline{\frac{1}{4} \text{ in.}}$$

Min preferable spacing of tie plates  
 $r_g$  of 1 L = 0.980 in.

$$\frac{12L}{0.980} = 300$$

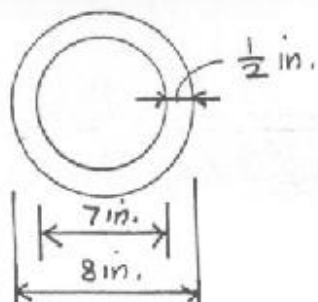
$$L = 24.5 \text{ ft Say } \underline{\underline{24 \text{ ft}}}$$

USE 4 Ls 5x5x $\frac{1}{2}$  with  
 $\frac{1}{4}$  x 12 x 1 ft 3 in. tie PLs  
@  $\phi$  of span.

✓ gcm

PROB # 5-2

Using the pipe section shown



$$A = \frac{(\pi)(8)^2}{4} - \frac{(\pi)(7)^2}{4} = 11.79 \text{ in.}^2$$

$$I = \frac{\pi d^4}{64} = \frac{(3.1416)(8)^4}{64} - \frac{(3.1416)(7)^4}{64} = 83.2 \text{ in.}^4$$

$$r = \sqrt{\frac{I}{A}} = \sqrt{\frac{83.2}{11.79}} = 2.66 \text{ in.}$$

(a) L = 30.0 ft

$$\frac{L}{r} = \frac{(12)(30)}{2.66} = 135.34 < 200 \text{ OK}$$

$$F_{cr} = \frac{(\pi)^2(29,000)}{(135.34)^2} = 15.63 \text{ ksi} < 36 \text{ ksi} \text{ OK}$$

$$P_{cr} = (15.63)(11.79) = \boxed{184.3 \text{ k}}$$

(b) L = 20.0 ft

$$\frac{L}{r} = \frac{(12)(20)}{2.66} = 90.23 < 200 \text{ OK}$$

$$F_{cr} = \frac{(\pi)^2(29,000)}{(90.23)^2} = 35.16 \text{ ksi} < 36 \text{ ksi} \text{ OK}$$

$$P_{cr} = (35.16)(11.79) = \boxed{414.5 \text{ k}}$$

(c) L = 15.0 ft

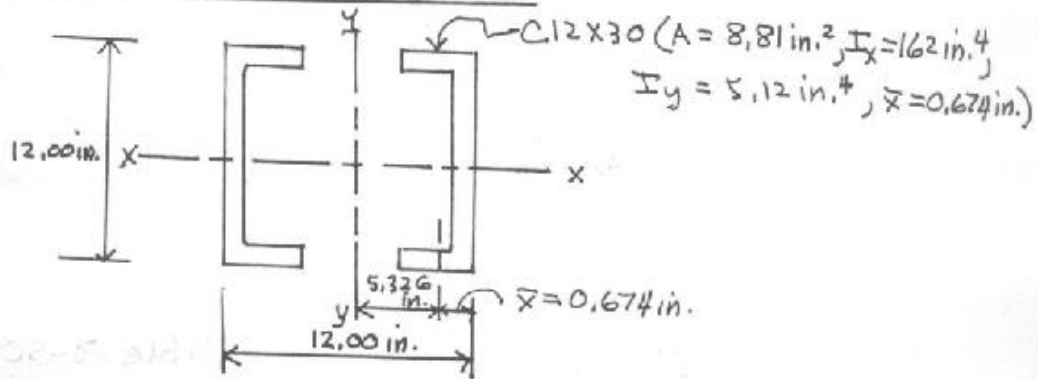
$$\frac{L}{r} = \frac{(12)(15)}{2.66} = 67.67 < 200 \text{ OK}$$

$$F_{cr} = \frac{(\pi)^2(29,000)}{(67.67)^2} = 62.50 \text{ ksi} > 36 \text{ ksi}$$

$\therefore$  Euler equation not applicable

PROB# 5-4

Using the section shown



$$A = (2)(8.81) = 17.62 \text{ in.}^2$$

$$I_x = (2)(162) = 324 \text{ in.}^4$$

$$I_y = (2)(5.12) + (2)(8.81)(5.326)^2 = 510 \text{ in.}^4$$

$$r_y = \sqrt{\frac{324}{17.62}} = 4.29 \text{ in.}$$

$$\frac{L}{r} = \frac{(12)(40)}{4.29} = 111.89$$

$$F_{cr} = \frac{(\pi)^2(29,000)}{(111.89)^2} = 22.86$$

$$P_{cr} = (22.86)(2 \times 8.81) = \boxed{402.8 \text{ k}}$$

✓ gcm

PROB# 5-6

Using a W14x30 ( $A_g = 8.85 \text{ in.}^2$ ,  $r_y = 1.49 \text{ in.}$ )

$$KL = (0.8)(18) = 14.4 \text{ ft}$$

$$\frac{K_y L_y}{r_y} = \frac{(12)(14.4)}{1.49} = 115.97$$

$\phi_c F_{cr} = 15.91 \text{ ksi}$  from Table 3-50 in  
AISC Specification (Part 16)

$$\phi_c F_{cr} = (15.91)(8.85) = \boxed{140.8 \text{ k}}$$

✓ gcm